

# INTERNATIONAL PIPELINE CONFERENCE

September 29 - October 3, 2008

2008

The Hyatt Regency Hotel & The TELUS Convention Centre, Calgary, Alberta, Canada



## Airborne Leak Detection

Prediction of Gas Transport Through Soil and Atmosphere

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October 3, 2008

# Outline

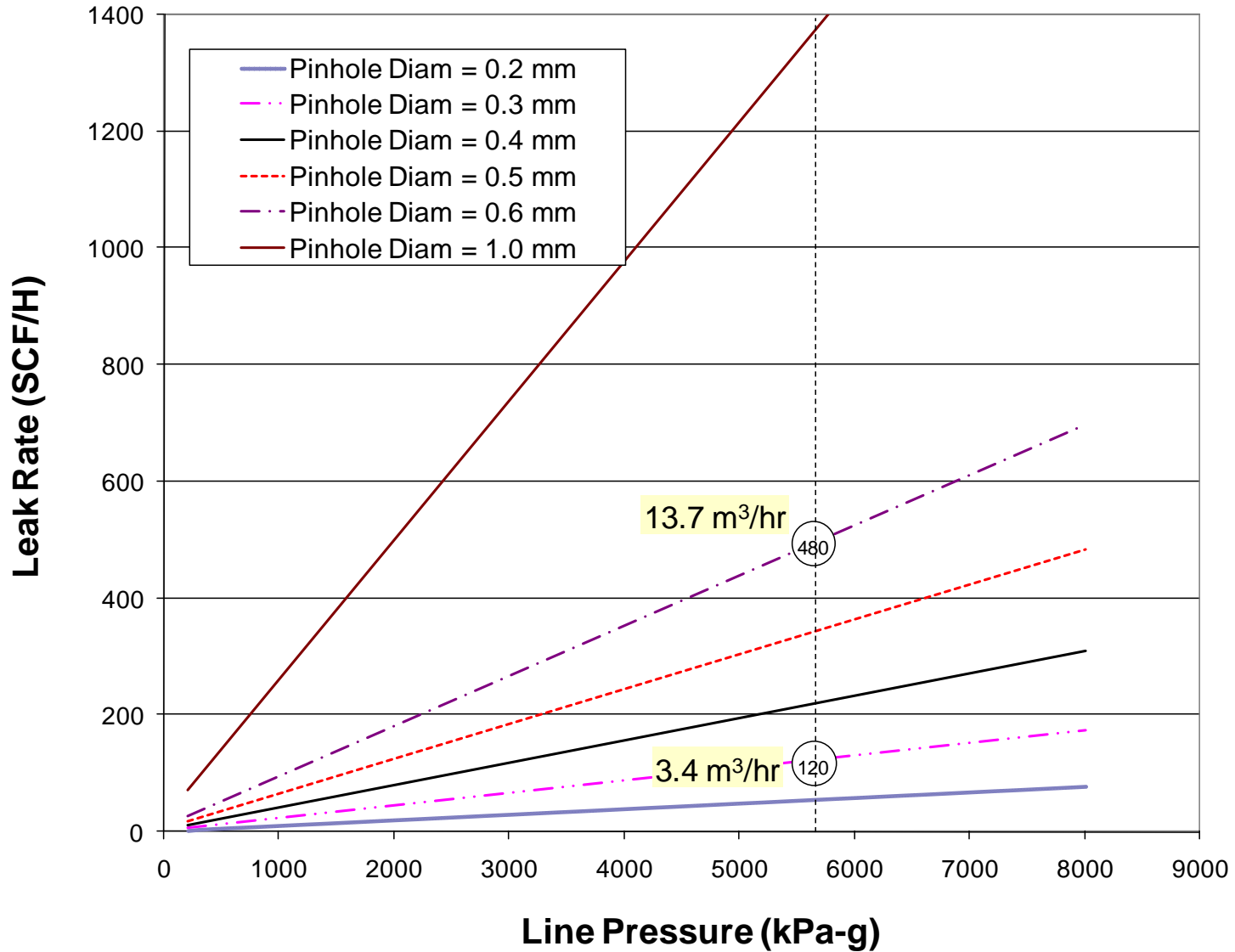
1. Motivation
2. Current Leak Detection Technologies
3. Advective Gas Transport Mechanism
4. Diffusive Gas Transport Mechanism
5. Simulation of Gas Transport (Atmosphere)
6. Field Test
7. Concluding Remarks

# Motivation

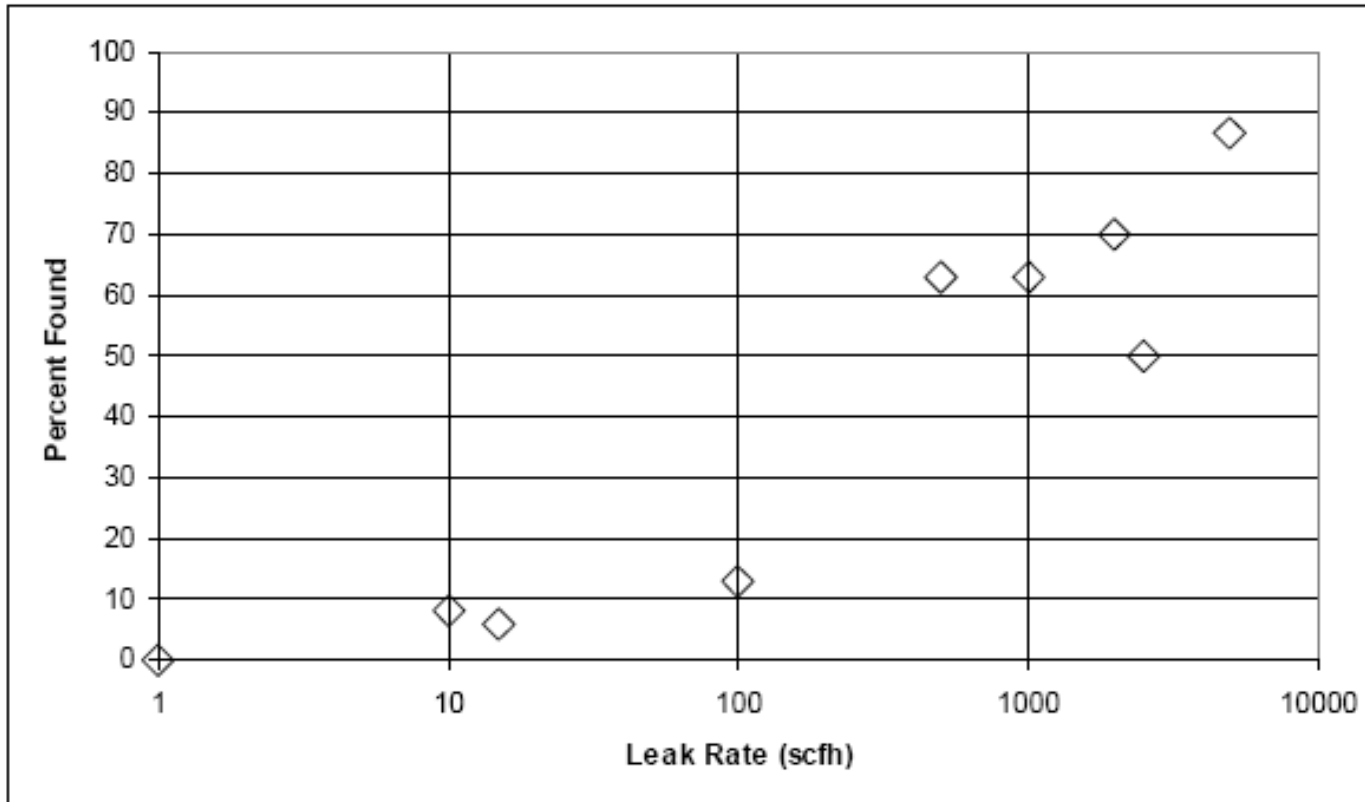
- Hydrotesting of newly constructed pipelines is required as per CSA Z662-07 Section 8.
- Cold weather construction challenges include: water freezing, availability of water, mixing water with methanol, and associated environmental concerns.



# Leak Rates



# DOE Round-Robin Test (2004)



Ref: Buckingham, J.C., Grimley, T.A., Burkey, R.C., "Field Testing of Remote Sensor Gas Leak Detection Systems," Southwest Research Institute®, Final Report for Department of Energy, Rocky Mountain Oilfield Testing Center, December 2004.

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# Technology Classifications

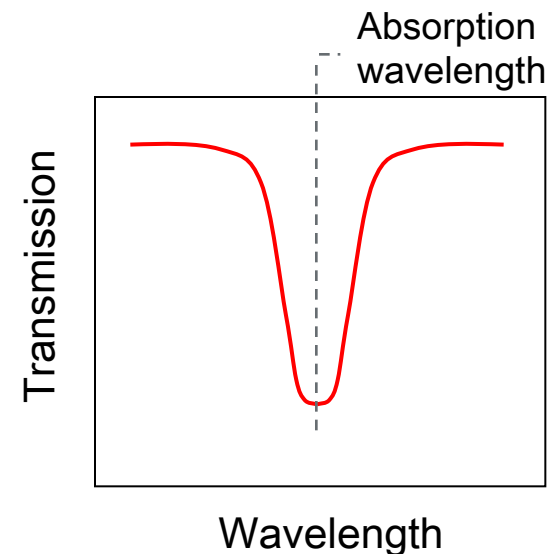
## Extractive sample-based technologies:

- ▶ **Combustible Gas Indicators (CGI):** catalytic combustion of gas sample
- ▶ **Flame Ionization Detectors (FID):** senses increase in ions in a hydrogen-burning flame, detects all combustible gases

## Optical-based technologies:

- ▶ **Passive**
- ▶ **Active (TDLA & DIAL)** 

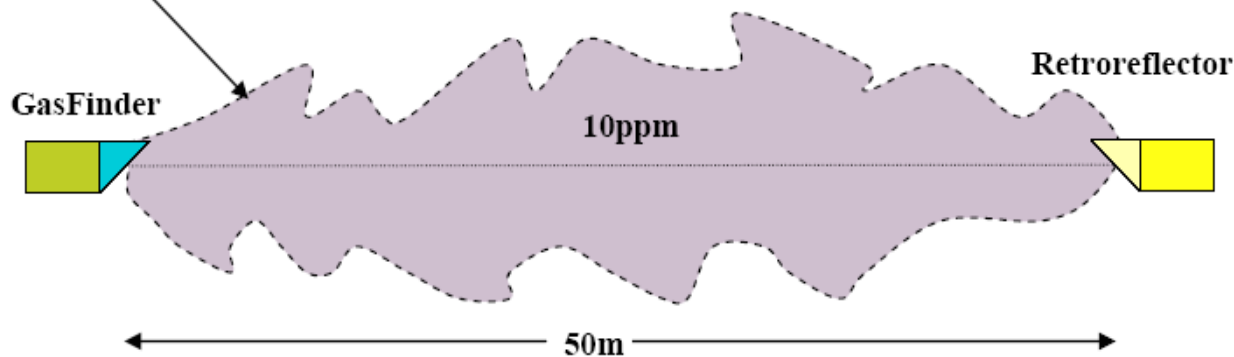
Beer-Lambert's law:  $\log_{10}(I_0/I) = A$



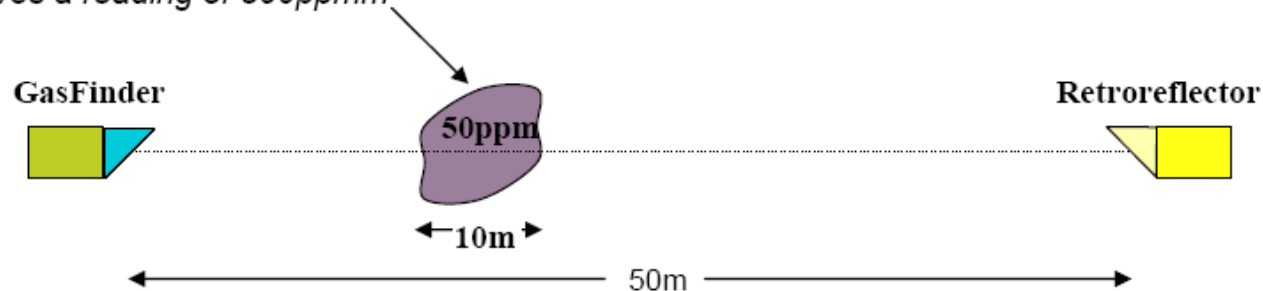
# Concentration Path Length

$$\text{Concentration Path Length} = \text{CPL} = \frac{\int C dL}{L}$$

A uniform background concentration of 10 ppm over 50m gives a reading of 500 ppm.



A concentrated cloud of 50 ppm, 10m in diameter, in a background of 0 ppm also gives a reading of 500ppm.

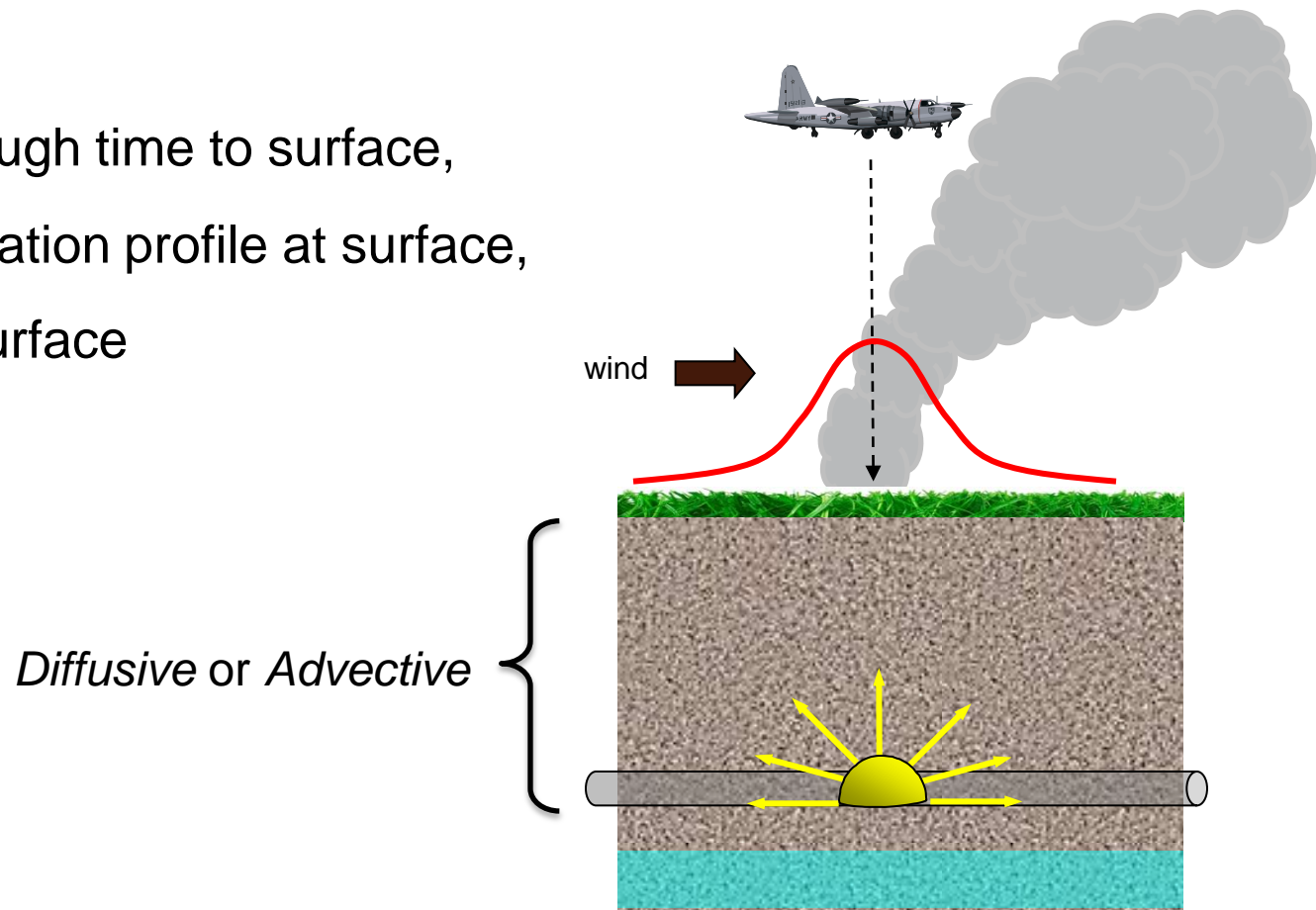


Courtesy of Boreal Laser Inc. 2003

# Approach

Determine:

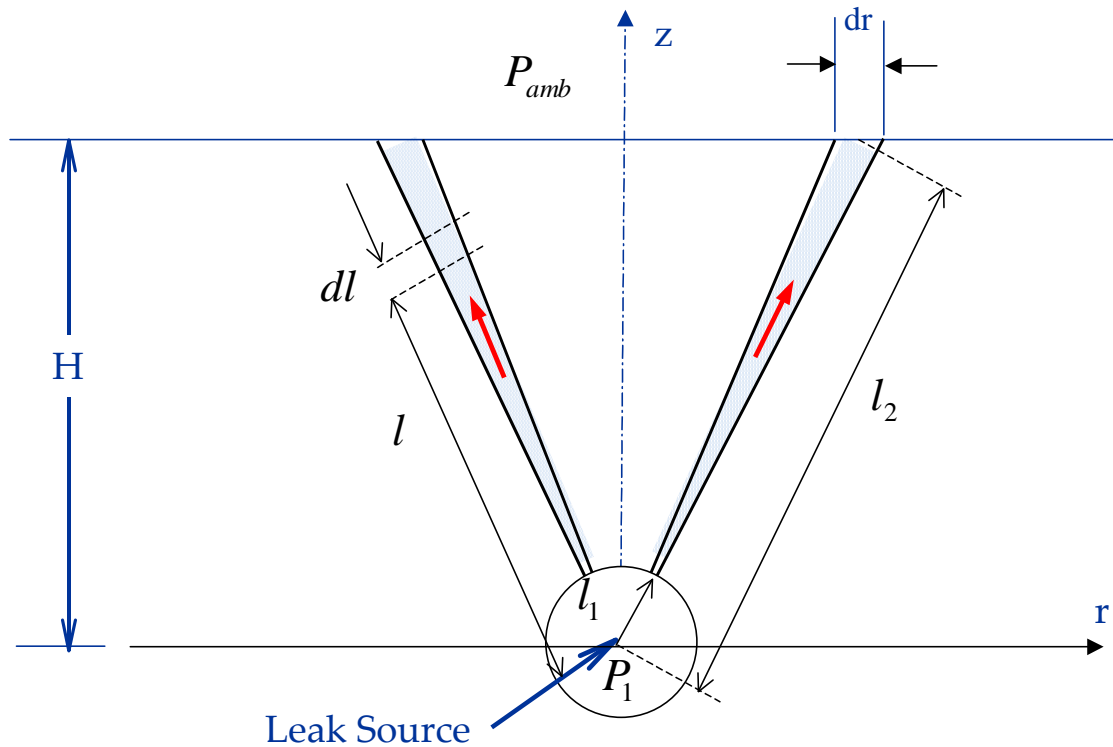
- Breakthrough time to surface,
- Concentration profile at surface,
- Flux at surface



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# Advective Flow Model



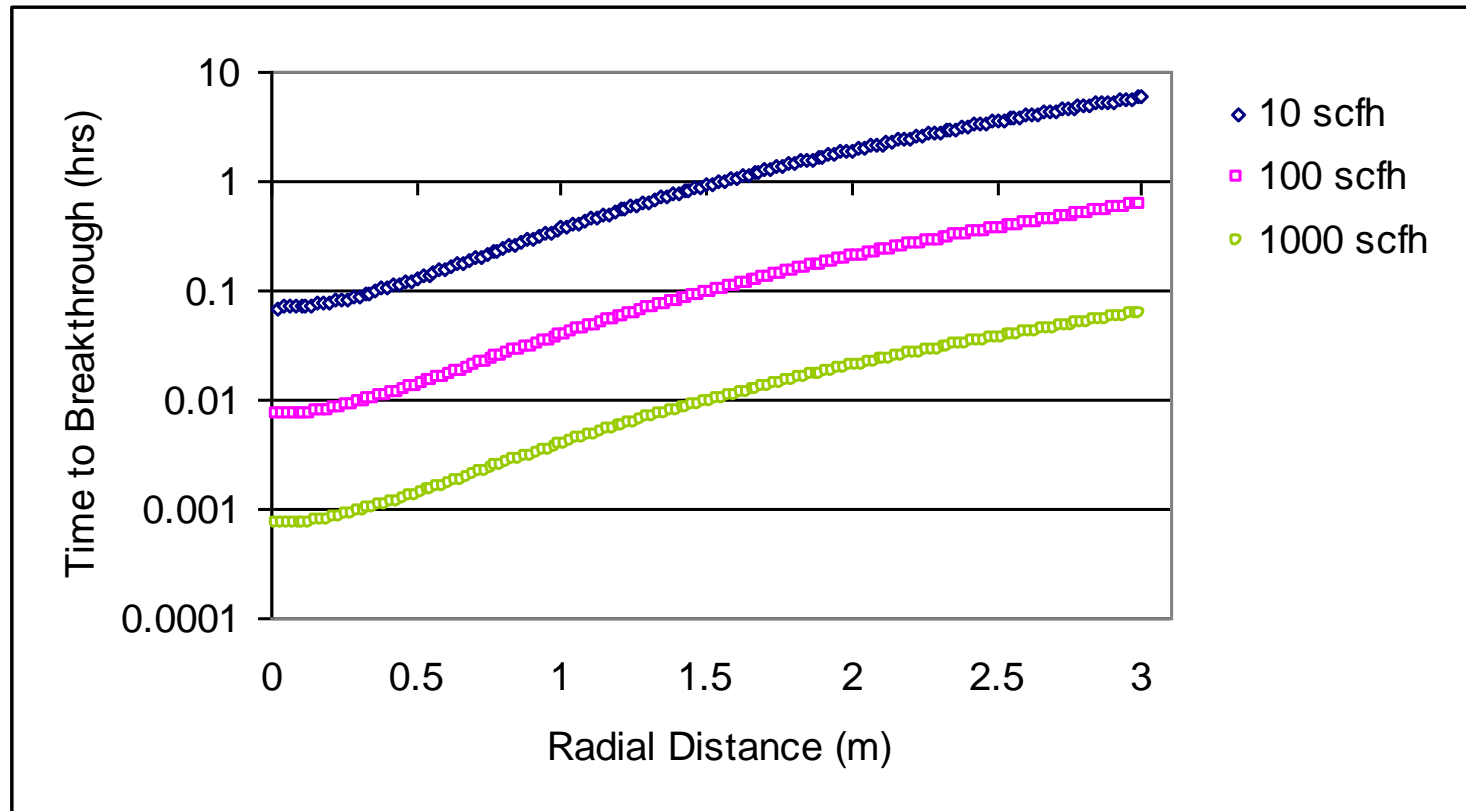
## Known:

- Total mass flux (leak rate)
- Soil properties

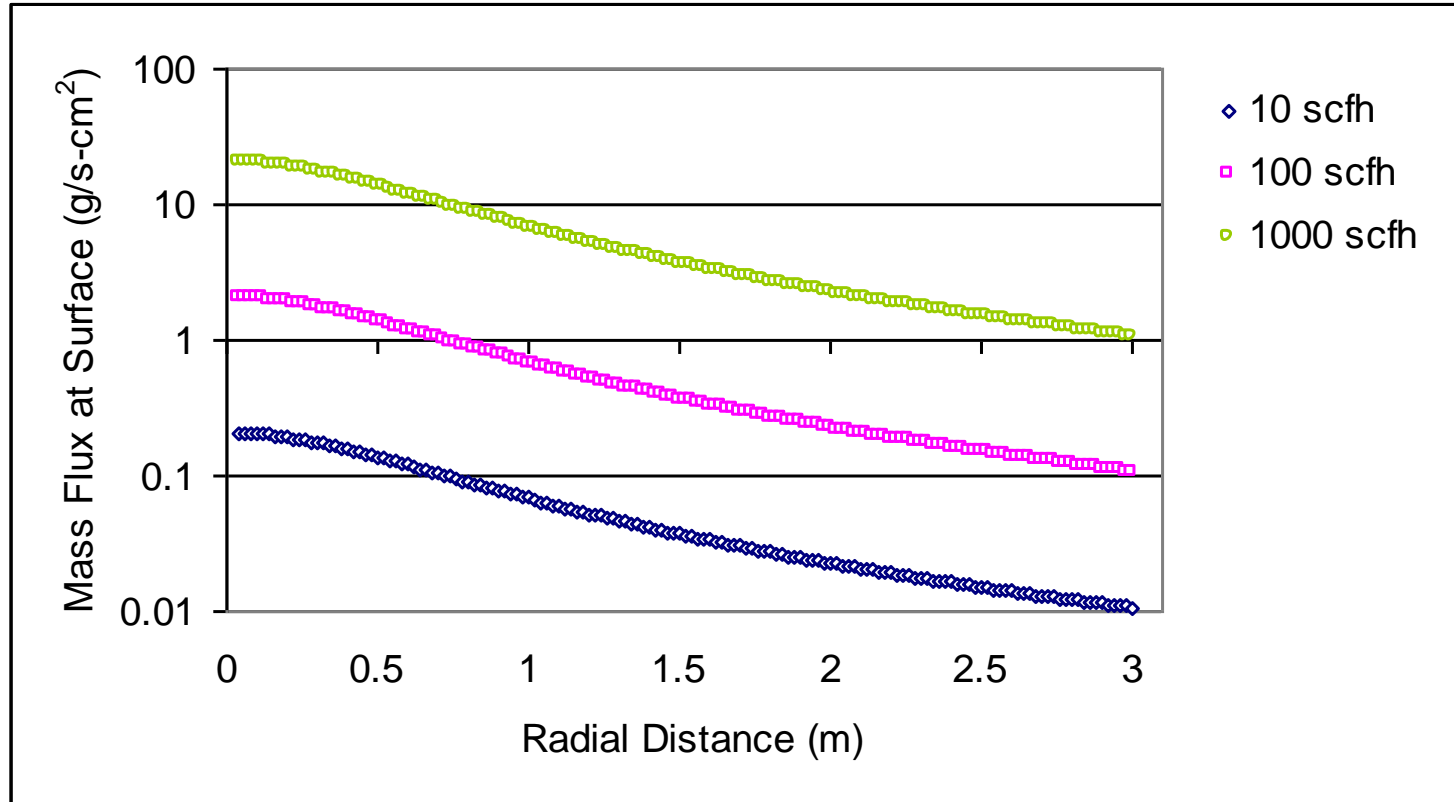
## Unknown:

- $dP$
- Mass flux profile
- Time to reach surface
- Surface velocity

# Time to Breakthrough (Depth = 0.7 m)



# Mass Flux at Surface (Depth = 0.7 m)



# Péclet Number

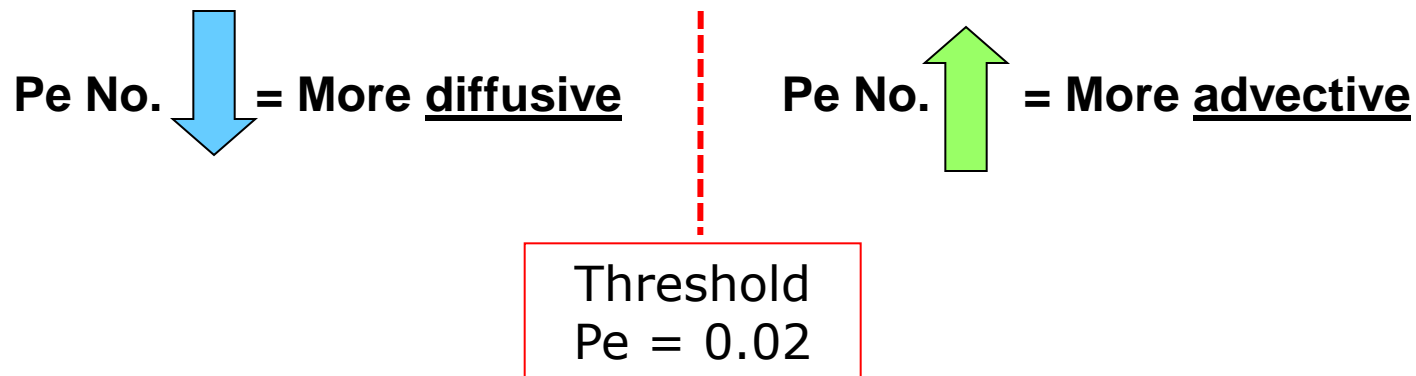
$$Pe \equiv \frac{\text{Advective flow velocity}}{\text{Diffusive flow velocity}} = \frac{v^o d}{D_{eff}}$$

Where

$v^o$  = Flow velocity (actual)

$d$  = Characteristic length (soil particle diameter)

$D_{eff}$  = Effective diffusion coefficient of gaseous methane in air



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# Diffusive Model Governing Equation

The transport model is based on Fick's 2<sup>nd</sup> Law:

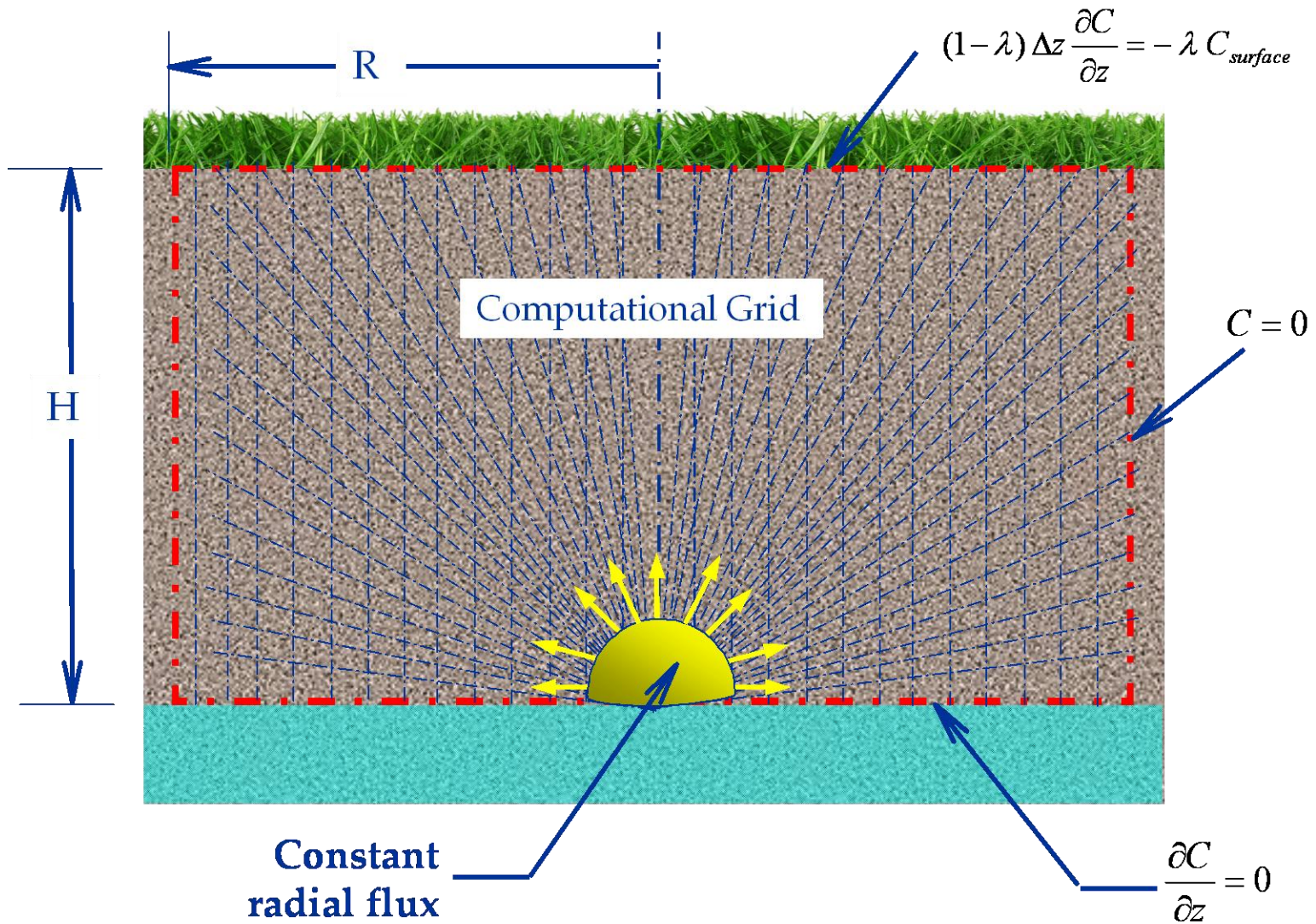
$$\frac{\partial C}{\partial t} = D \nabla^2 C$$

The mass flux is:

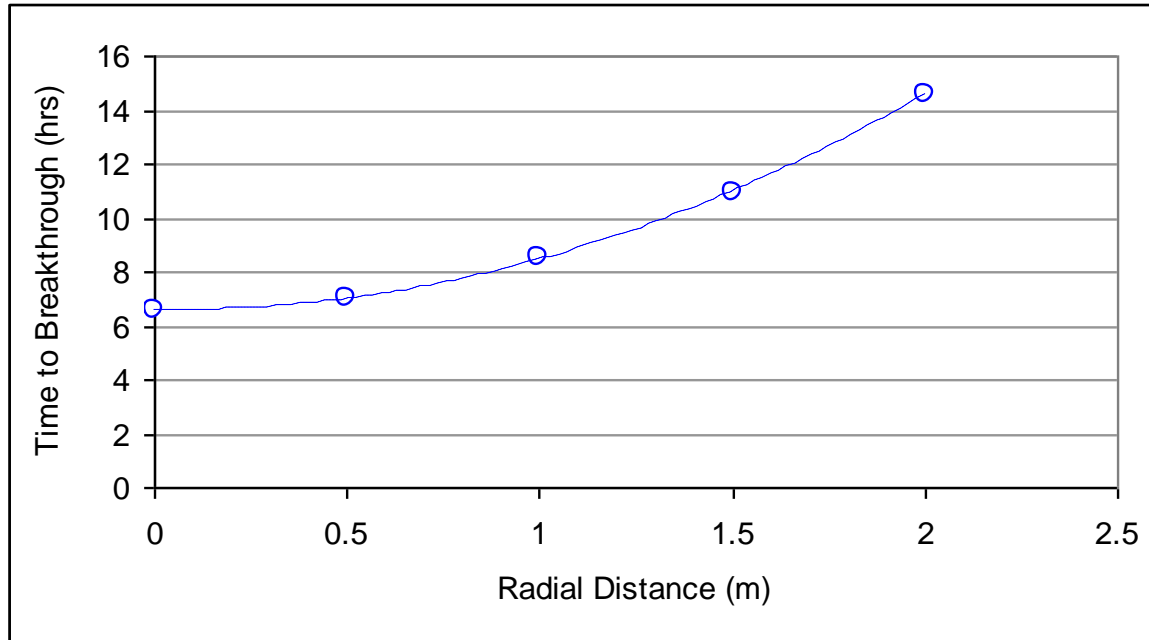
$$J = -D \nabla C$$

This was solved through numerical simulation in R-UNSAT.

# Boundary Conditions



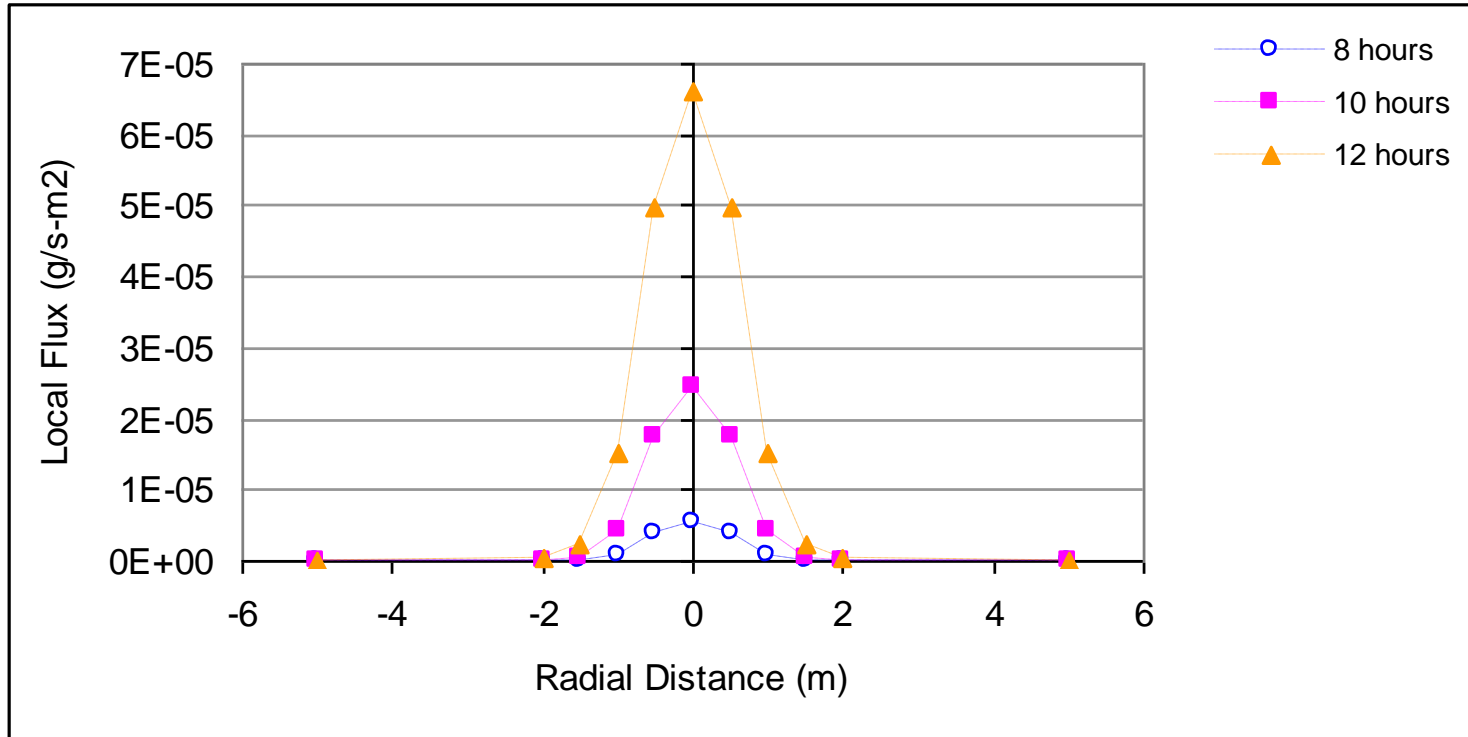
# Diffusive Model Breakthrough Times



*Breakthrough time is the time at which methane concentrations are greater than the atmospheric value of 1.75 ppm.*

Depth = 2 m, Q = 10 scfh, Porosity = 0.35

# Mass Flux at Surface



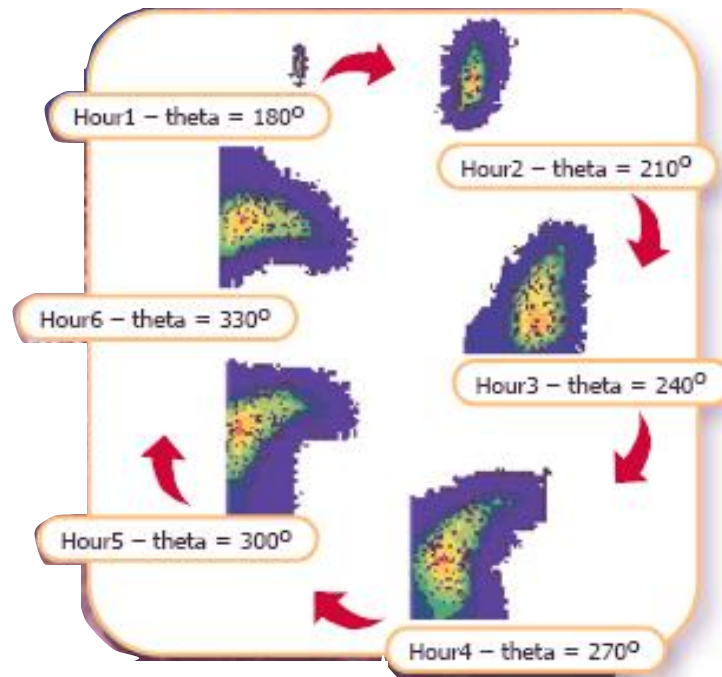
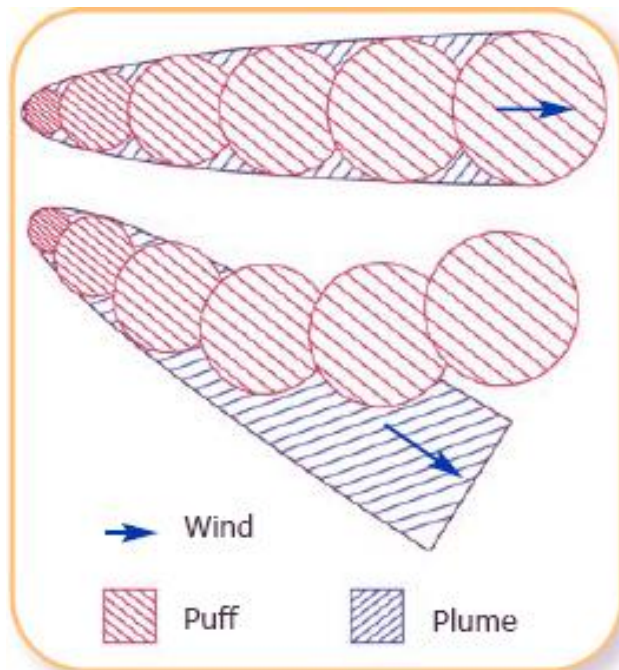
Depth = 2 m, Q = 10 scfh, Porosity = 0.35.

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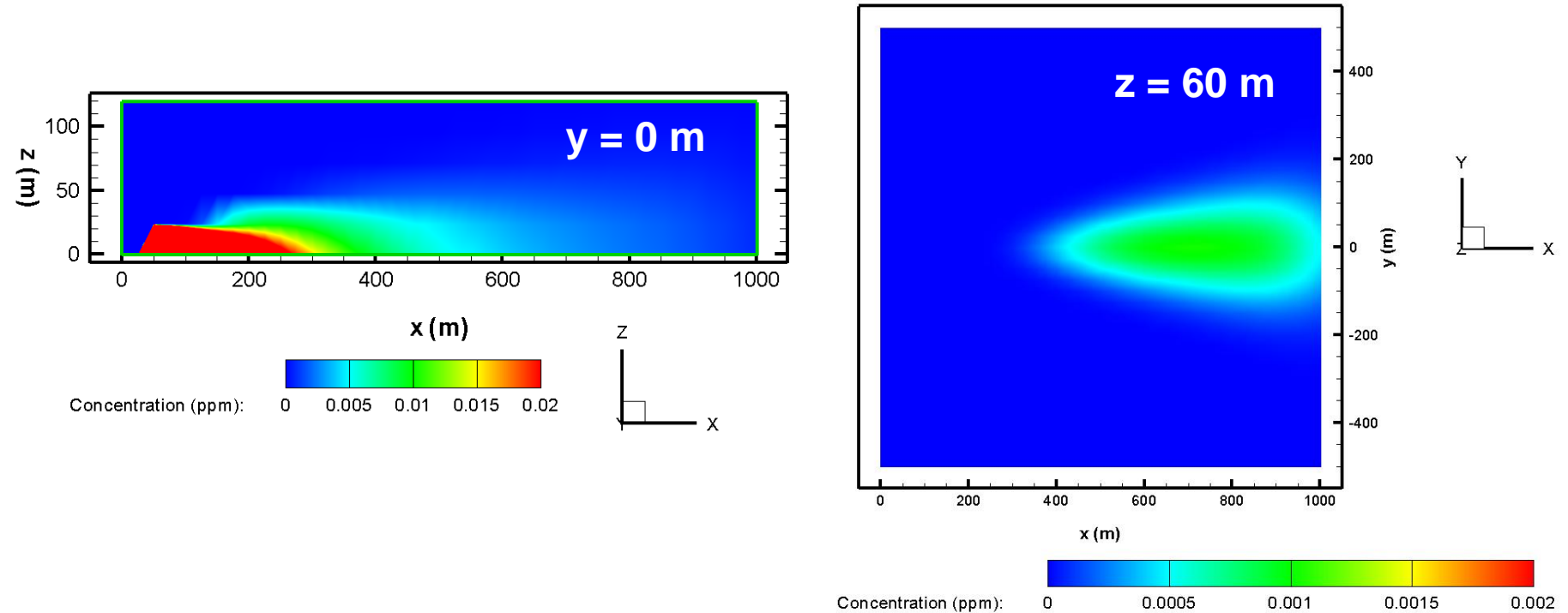
# Numerical Simulation: CALPUFF

CALPUFF is a **non-steady-state** emissions modeling program developed by the US Environmental Protection Agency.



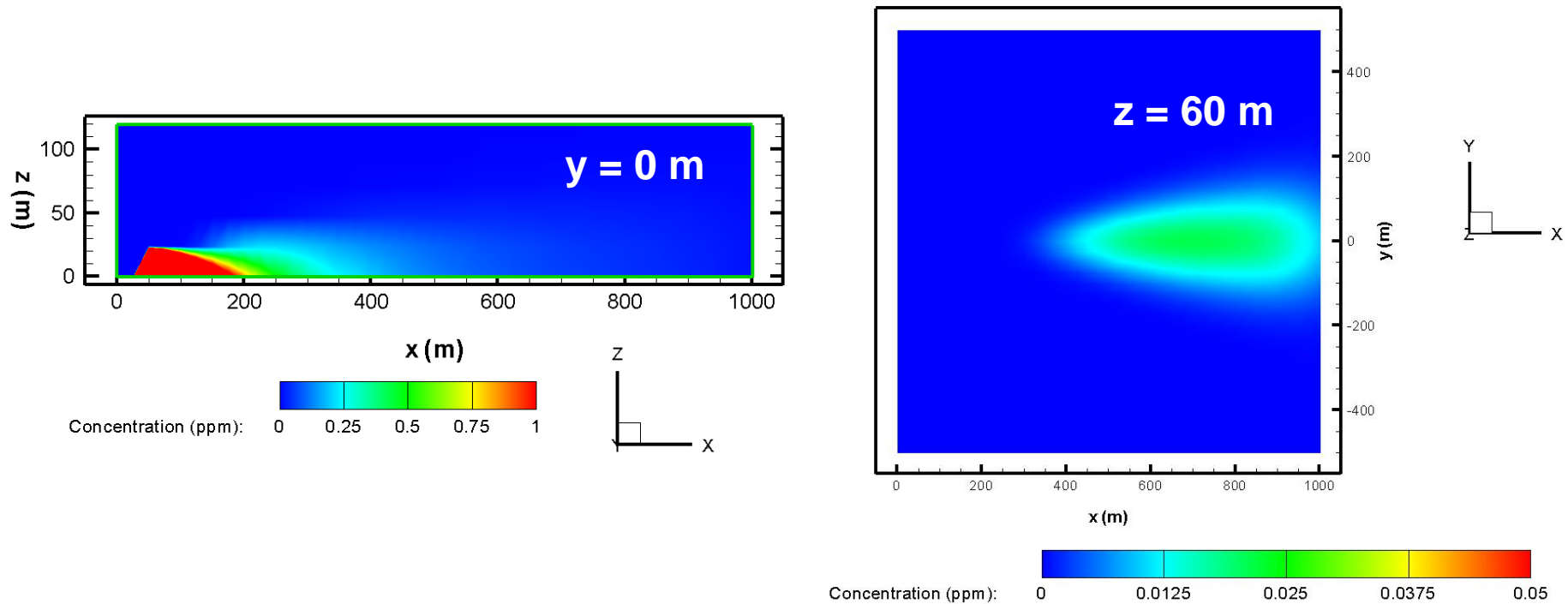
© 1996-2007 Lakes Environmental Software

# 10 scfh leak, 3 hrs since initiation



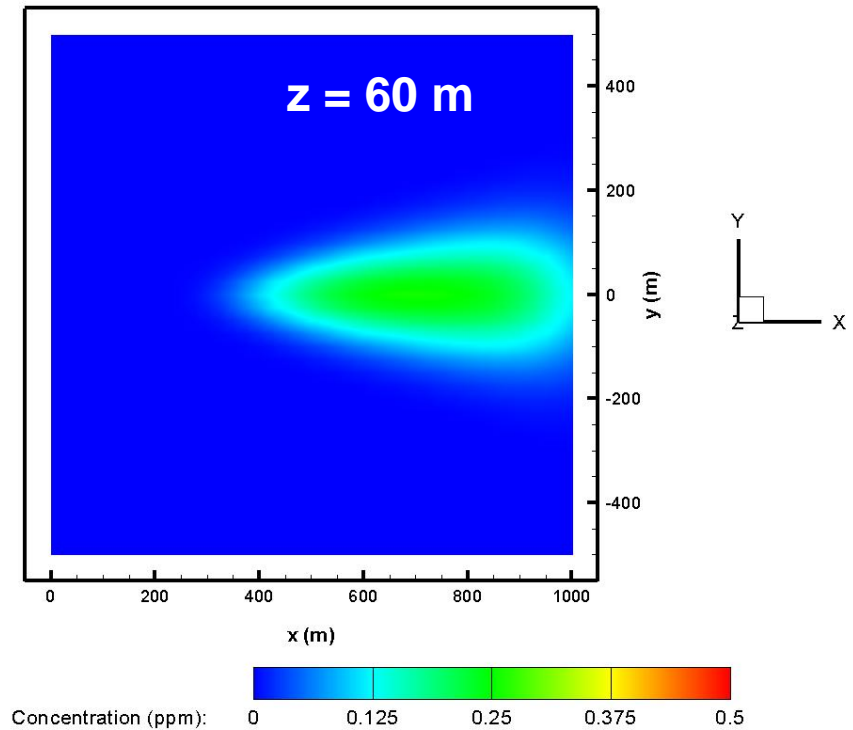
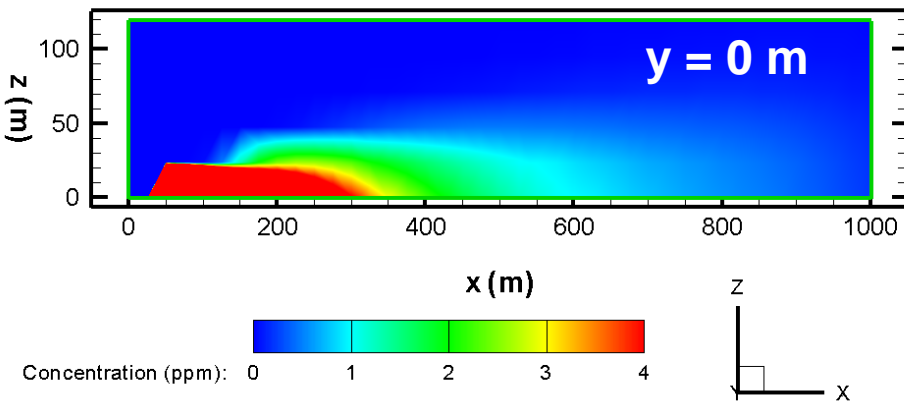
Depth = 0.7 m,  $Q = 10$  scfh, Porosity = 0.35.

# 100 scfh leak, 1 hr since initiation



Depth = 0.7 m,  $Q = 100$  scfh, Porosity = 0.35.

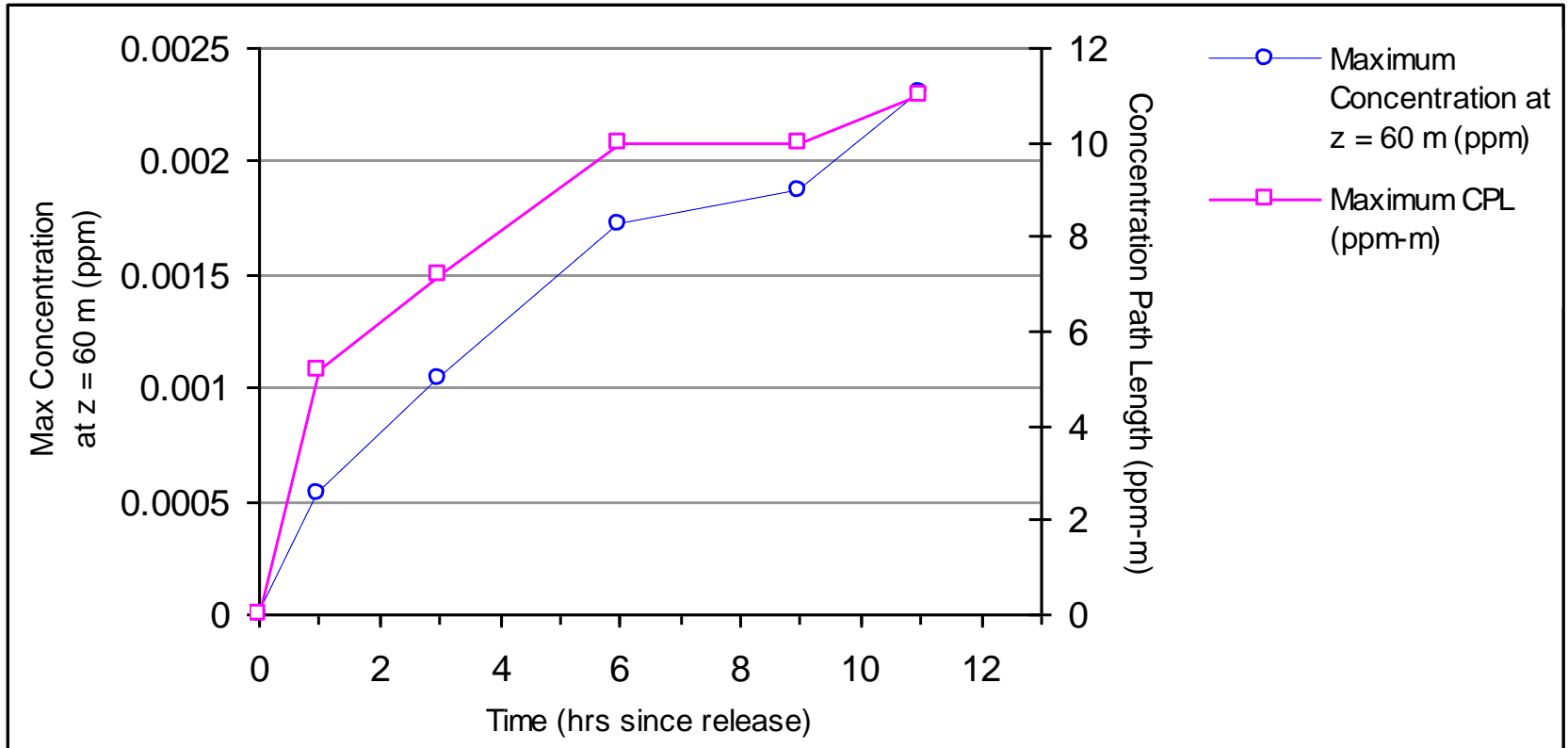
# 1,000 scfh leak, 0.5 hr since initiation



Depth = 0.7 m,  $Q = 1,000$  scfh, Porosity = 0.35.

# Maximum Local Concentration and CPL

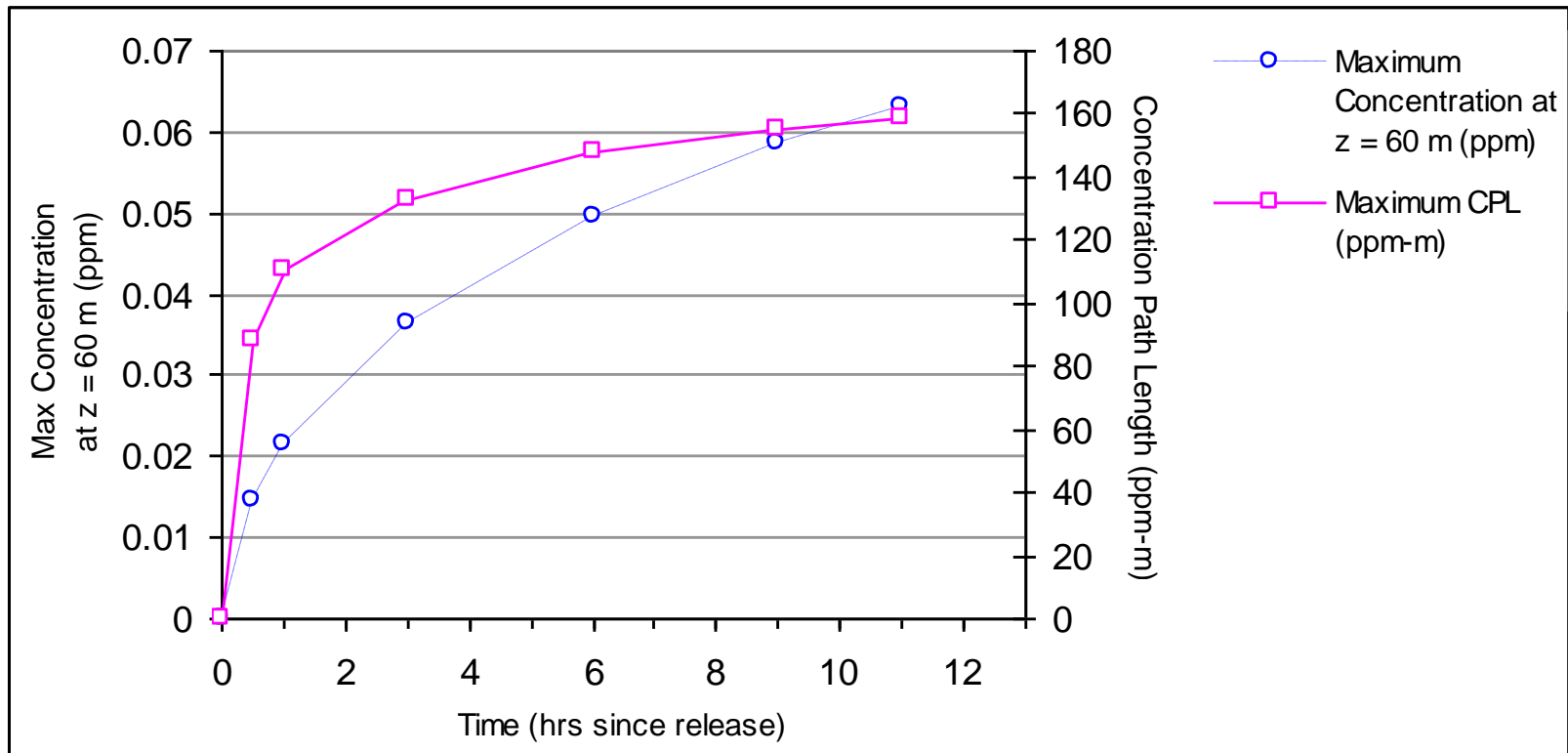
## Q = 10 scfh



Local concentration taken at z = 60 m.  
CPL from x = 0-1,000m and z = 0-400m.  
Depth = 0.7 m, Q = 10 scfh, Porosity = 0.35.

# Maximum Local Concentration and CPL

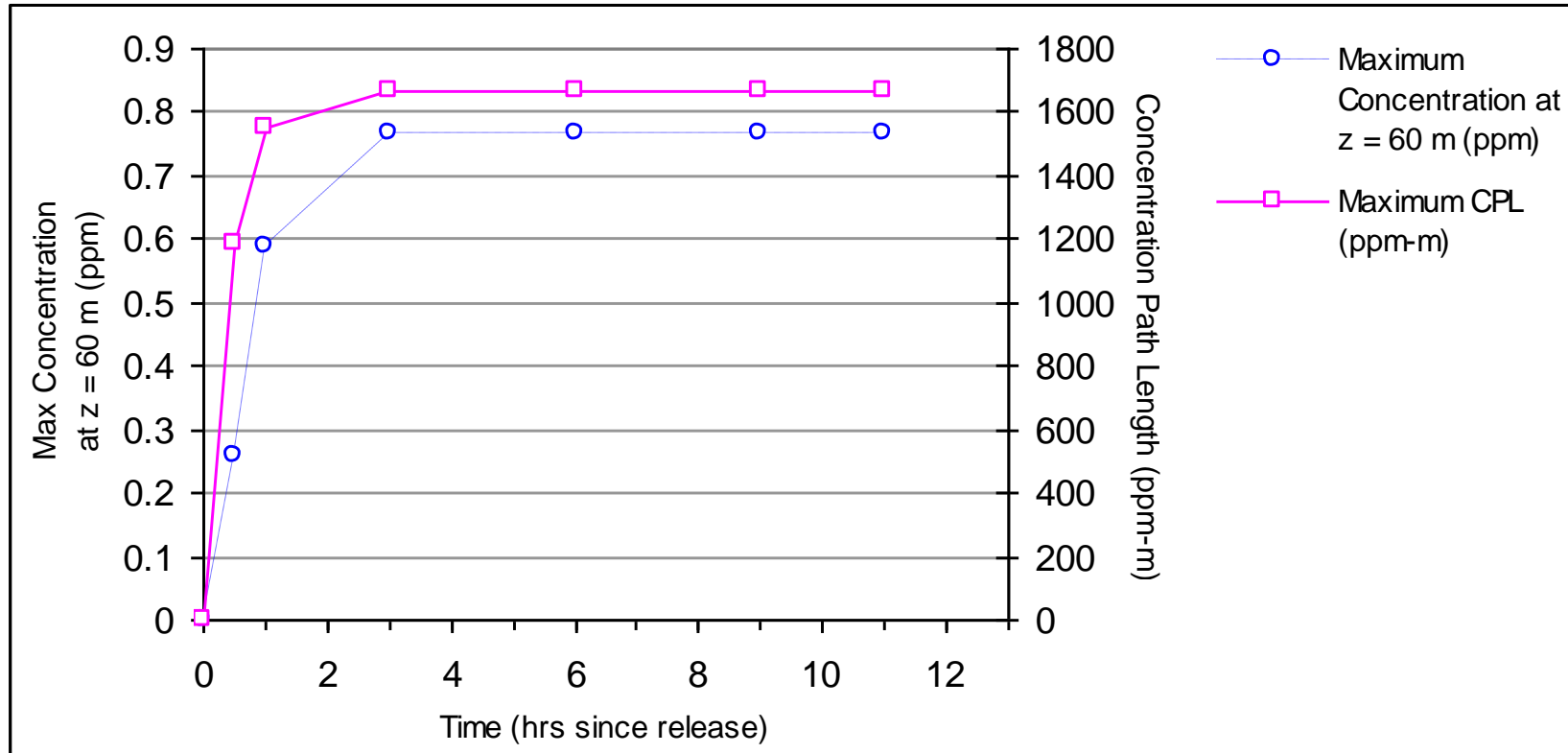
## Q = 100 scfh



Local concentration taken at z = 60 m.  
CPL from x = 0-1,000m and z = 0-400m.  
Depth = 0.7 m, Q = 100 scfh, Porosity = 0.35.

# Maximum Local Concentration and CPL

## Q = 1,000 scfh

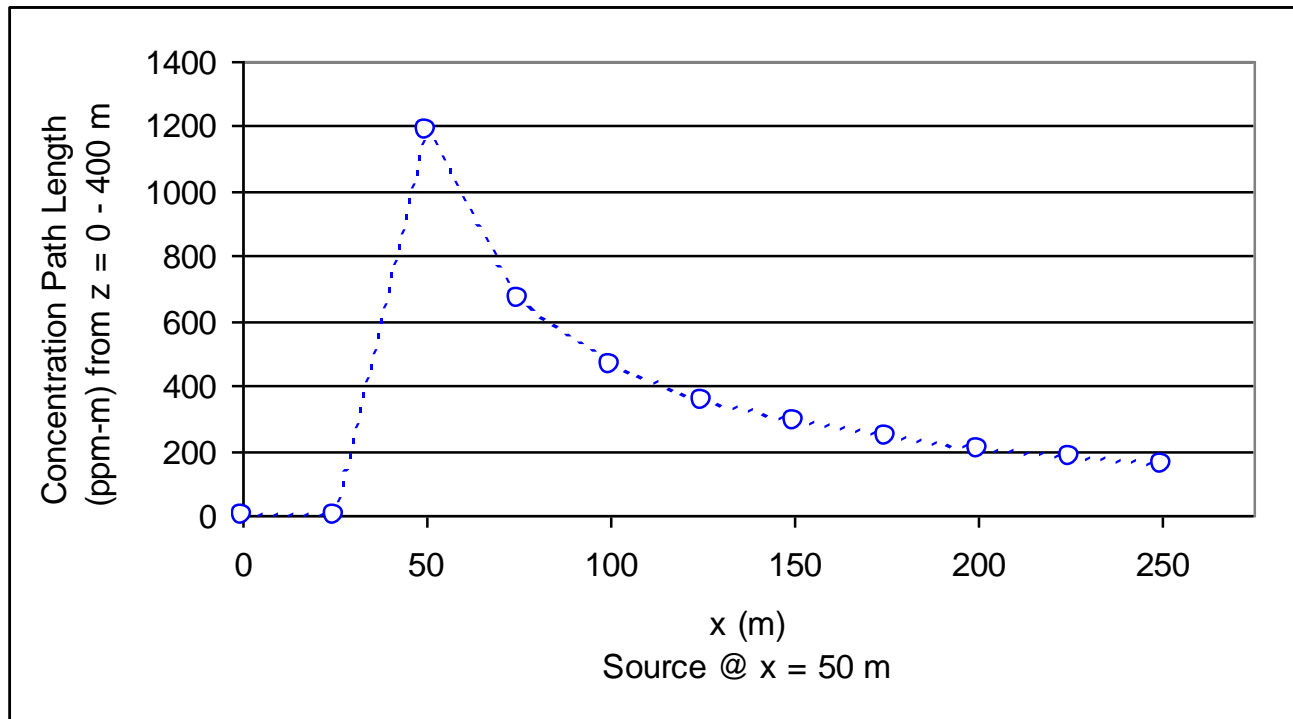


Local concentration taken at z = 60 m.

CPL from x = 0-1,000m and z = 0-400m.

Depth = 0.7 m, Q = 1,000 scfh, Porosity = 0.35.

# CPL Profile Along Plume Path

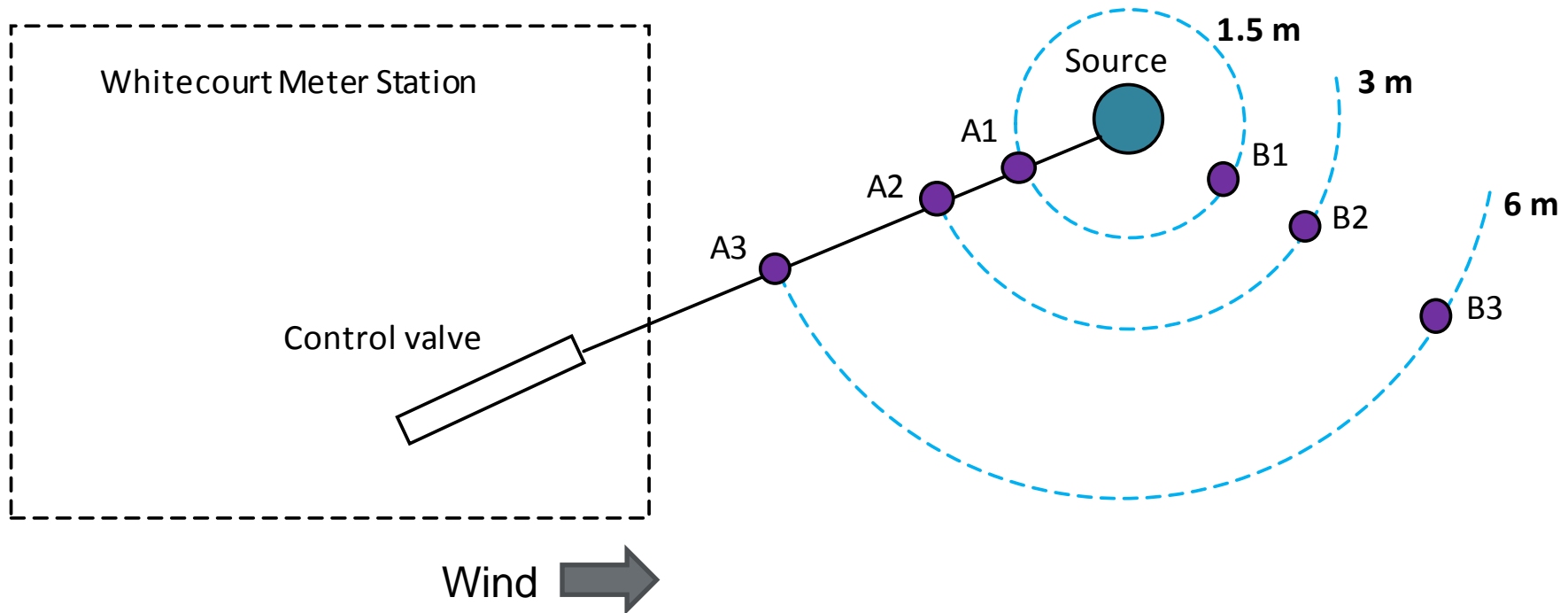


Depth = 0.7 m, Q = 1,000 scfh, Porosity = 0.35, 0.5 hrs of leakage.

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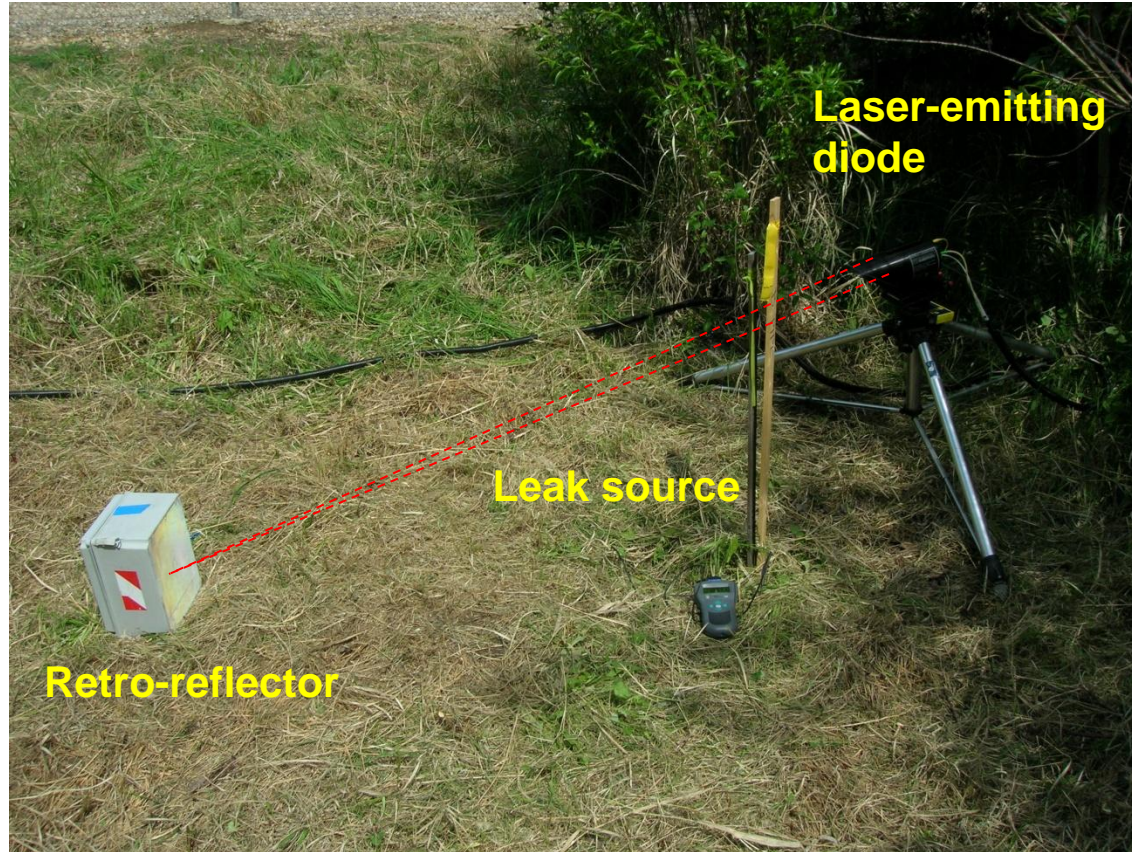
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# Field Test: Artificial Leak Site Schematic



Depth = 0.7 m, Q = 190 scfh, Porosity = 0.35.

# Field Test: Equipment



# Field Measurements

| Location                        | Time since leak initiation | Approximate concentration         | Transport regime modeled | Predicted breakthrough time |
|---------------------------------|----------------------------|-----------------------------------|--------------------------|-----------------------------|
| Whitecourt<br>Above source      | 10 s                       | Unknown (saturated equipment)     | Advective                | 22 s                        |
| Whitecourt<br>A1 (1.5 m upwind) | 2 min                      | 200 ppm <sub>v</sub> <sup>1</sup> | Diffusive                | 1 hr 43 min                 |
| Whitecourt<br>A2 (3 m upwind)   | 3 min                      | 50 ppm <sub>v</sub> <sup>1</sup>  | Diffusive                | > 5 hrs                     |
| Whitecourt<br>A3 (6 m upwind)   | 4 min                      | 10 ppm <sub>v</sub> <sup>1</sup>  | Diffusive                | > 5 hrs                     |
| Blueridge<br>Above source       | 18 s                       | 900 ppm <sub>v</sub>              | Advective                | 1 min 51 s                  |

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# Concluding Remarks

| Leak Rate  | Wind Speed | Stability         | Minimum Time to Steady State Plume |
|------------|------------|-------------------|------------------------------------|
| 10 scfh    | 5 m/s      | Slightly Unstable | <b>9 hrs</b>                       |
| 1,000 scfh | 5 m/s      | Slightly Unstable | <b>3 hrs</b>                       |

1. Numerical models are conservative.
2. Soil-transport model breakthrough times agree within reason to measured results.
3. Flying altitude, meteorological conditions and technology requirements should be considered when determining 'wait time'.

# Acknowledgment

TransCanada:

Rachel Lee

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John Selby

Hamish Adam

Edwin Thornton

ITT:

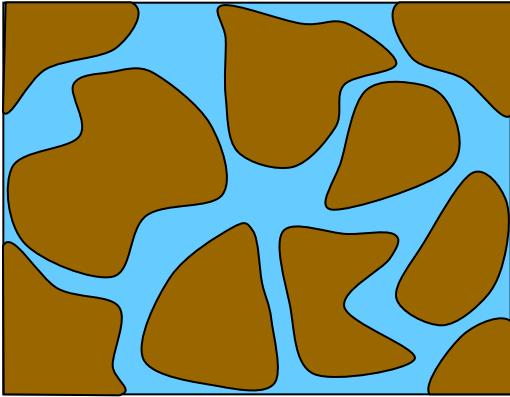
Steve Stearns

Rosen Canada:

Daryl Ronsky

# Supporting Information

# Soil Properties



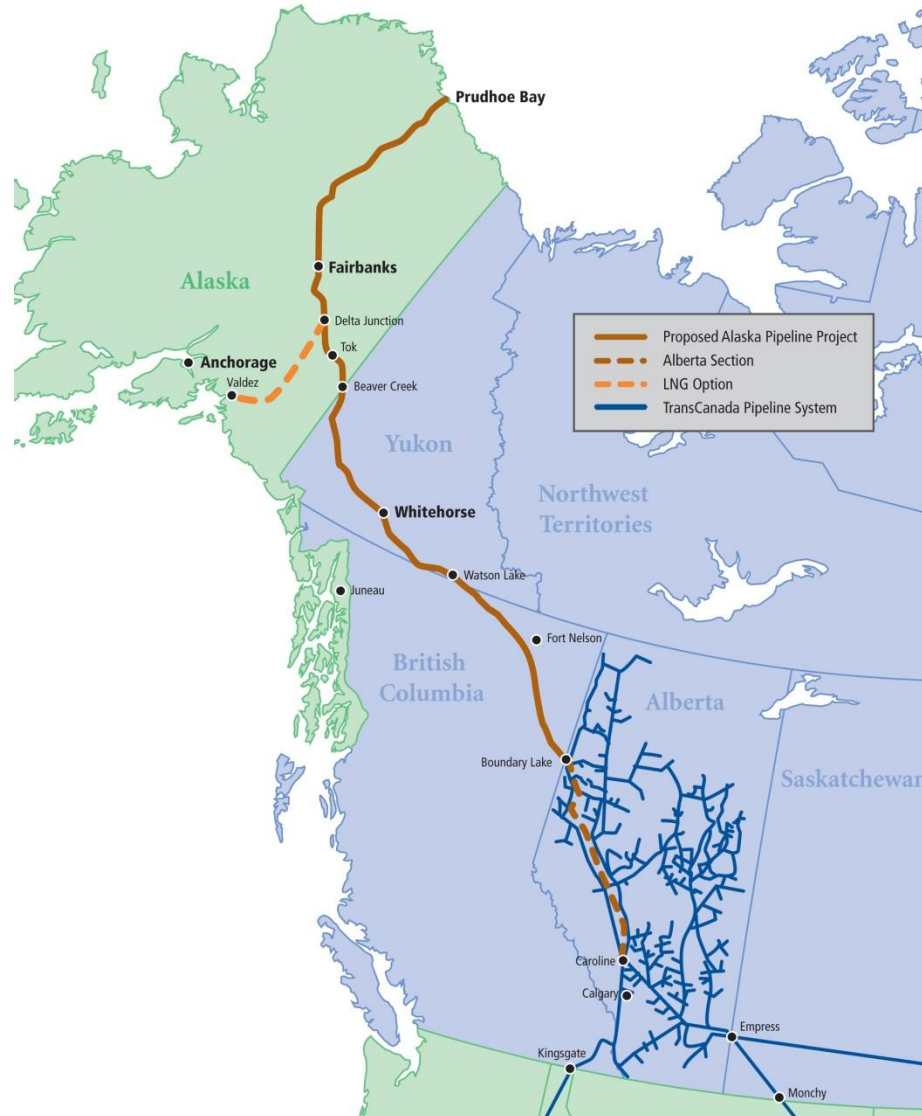
Porosity = 0.35 – 0.50

Moisture Content = 5%

Soil Temperature = 10°C

Ambient Pressure = 760 mm Hg

# Alaska Pipeline



# Modelling Properties

The following are additional parameters used in the simulation:

- $e_a = 30\%$
- $e_t = 35\%$
- $d_e = 0.0015$  mm
- Soil temperature =  $0^\circ\text{C}$
- Ambient Pressure = 698 mm Hg
- $V_x = 5$  m/s at 10 m elevation above ground.
- Mixing height = 1000 m above ground.
- Stability class during test was assumed slightly unstable (Pasquill-Gifford Class C).
- Leak rates: 0.283, 2.83 and 28.3 m<sup>3</sup>/hr (10, 100, and 1,000 scfh)

At these three rates and at 0.7 m depth, the gas transport mechanism through the soil was found to be predominantly advective as the  $Pe$ 's at  $R = 0$  for these three rates were 0.3, 3 and 30, respectively.

# Field Test Schematic

